

PROPERTIES OF PORTLAND BLAST FURNACE SLAG CEMENT PRODUCED USING PHOSPHOGYPSUM

513 (00)
FURNACE SLAG CEMENT

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INTRODUCTION

Extensive work carried out in Japan on Japanese phosphogypsum has shown that when phosphogypsum produced by the dihydrate process was used to control the setting time of cement, the impurities (phosphate, fluoride and organic matter) present in the phosphogypsum considerably influenced the setting time and early strength development.

Not only the setting time of cement was found to be greatly retarded but there was also a marked reduction in its early strength. Investigations carried out in other countries suggest that beneficiated phosphogypsum can be used in place of mineral gypsum without any adverse effect.

India produces about 1.5 million tonnes of phosphogypsum every year. Some work on the use of beneficiated phosphogypsum produced in India as a set retarder in cement has already been reported.

The properties of portland cement prepared in the laboratory by intergrinding portland cement clinker and granulated blast furnace slags with unprocessed and processed phosphogypsum samples are described here.

EXPERIMENTAL

Materials used

1. Phosphogypsum : It was procured from M/S Coro-

mondal Fertilizer Ltd., Vishakhapatnam. Its chemical composition is shown in Table 1.

Table 1

Chemical Analysis of Phosphogypsum

| Constituents | Percentage |
|---|------------|
| Total P ₂ O ₅ | 0.65 |
| Water-Soluble P ₂ O ₅ | 0.29 |
| Crystal lattice-Substituted P ₂ O ₅ | 0.33 |
| Insoluble P ₂ O ₅ | 0.03 |
| Total F | 0.44 |
| Water-Soluble F | 0.28 |
| Organic Matter | 0.11 |
| SiO ₂ | 5.14 |
| R ₂ O ₃ | 0.85 |
| CaO | 31.47 |
| MgO | 0.43 |
| Na ₂ O | 0.32 |
| SO ₃ | 41.98 |
| H ₂ O | 19.78 |

The phosphogypsum was of high purity (90.25%). It was used as such and after beneficiation by the wet sieve analysis technique¹⁰. The fraction passing 150 micron IS sieve was used.

2. Portland Cement Clinker : It was procured from M/S Orissa Cement Company, Rajgangpur. Its chemical composition is shown in Table 2.

Table 2

Chemical composition of cement clinker

| Constituents | Percentage |
|--------------------------------|------------|
| SiO ₂ | 23.29 |
| Al ₂ O ₃ | 5.63 |
| Fe ₂ O ₃ | 1.90 |
| CaO | 63.56 |
| MgO | 4.30 |
| SO ₃ | — |
| L.O.I. | 1.10 |

3. Granulated Blast Furnace Slags : The granulated blast furnace slag samples numbered A, B, C, D, E & F were received from M/S Hindustan Steel Ltd., Rourkela. Their chemical composition is shown in Table 3.

Hydraulic indices employed for evaluating potential hydraulicity of slags as recommended in IS: 455-1976 and computed from Chemical Composition are shown in Table 4.

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Table 5

Properties of PPS cement produced using mineral setonite gypsum

| Slag Designation | PPS cement composition | | | Normal consistency (%) | Setting Time (minutes) | | Compressive Strength (kg/cm ²) | | | | Autoclave Expansion (%) | |
|---------------------|------------------------|-----|----|------------------------|------------------------|-------|--|-----|-----|-----|-------------------------|------|
| | S* | C | G* | | Initial | Final | 1d | 3d | 7d | 28d | | 99d |
| A | 40 | 60 | 5 | 23.5 | 180 | 230 | 150 | 242 | 437 | 484 | 670 | 0.20 |
| | 50 | 50 | 5 | 24.5 | 235 | 290 | 146 | 224 | 367 | 478 | 650 | 0.22 |
| B | 40 | 60 | 5 | 23.2 | 170 | 200 | 128 | 208 | 333 | 514 | 666 | 0.46 |
| | 50 | 50 | 5 | 24.0 | 210 | 275 | 130 | 203 | 290 | 456 | 572 | 0.5 |
| C | 40 | 60 | 5 | 23.2 | 170 | 230 | 115 | 192 | 294 | 422 | 682 | 0.32 |
| | 50 | 50 | 5 | 24.2 | 285 | 355 | 108 | 180 | 277 | 394 | 510 | 0.51 |
| D | 40 | 60 | 5 | 23.5 | 215 | 245 | 122 | 202 | 290 | 434 | 640 | 0.31 |
| | 50 | 50 | 5 | 23.7 | 190 | 255 | 110 | 178 | 182 | 366 | 610 | 0.41 |
| E | 40 | 60 | 5 | 24.2 | 145 | 215 | 171 | 285 | 409 | 417 | 508 | 0.22 |
| | 50 | 50 | 5 | 25.5 | 160 | 210 | 156 | 225 | 321 | 528 | 576 | 0.26 |
| F | 40 | 60 | 5 | 25.5 | 150 | 195 | 142 | 238 | 345 | 389 | 660 | 0.21 |
| | 50 | 50 | 5 | 25.0 | 165 | 197 | 133 | 206 | 355 | 391 | 519 | 0.24 |
| | 0 | 100 | 5 | 22.0 | 180 | 225 | 144 | 260 | 305 | 592 | 611 | 0.51 |
| IS: 455-1976 Limits | | | | — | 30 | 600 | — | 160 | 220 | — | — | 0.80 |

* S = slag; C = cement clinker; G = Mineral Setonite Gypsum.

Preparation and testing of PBFS cement

Slag samples and cement clinker were interground in the proportions of 40:60 and 50:50 with 5% of unprocessed and processed phosphogypsum to a fineness of about 4,000 cm²/g (Blaine's). For comparative tests, a portland cement sample was also prepared by grinding cement clinker with 5% of high purity mineral gypsum (97.75%).

The cements produced were tested for physical properties by the methods specified in IS : 4031-1968²⁰.

RESULTS & DISCUSSION

Properties of PBFS cement

- a) With Mineral Gypsum : The effect of mineral gypsum on the physical properties of PBFS cement is shown in Table 5 (P.26). It can be seen that the experimental PBFS cement samples produced complied with setting and strength requirements of IS : 455-1976²¹.

Table 3

Chemical composition of blast furnace slags, Rourkela

| Constituents | Composition in % | | | | | |
|--------------------------------|------------------|-------|-------|-------|-------|-------|
| | A | B | C | D | E | F |
| SiO ₂ | 30.00 | 33.8 | 36.40 | 36.00 | 33.00 | 34.00 |
| FeO | 0.72 | 0.70 | 0.69 | 0.46 | 1.29 | 2.10 |
| Fe ₂ O ₃ | — | — | — | — | 1.42 | 0.43 |
| Al ₂ O ₃ | 26.80 | 22.87 | 24.60 | 24.64 | 21.54 | 25.90 |
| CaO | 31.50 | 32.50 | 29.50 | 27.50 | 33.30 | 27.80 |
| MgO | 7.32 | 6.12 | 5.76 | 5.94 | 3.76 | 2.90 |
| MnO | 2.29 | 3.30 | 2.40 | 4.83 | 4.94 | 6.17 |
| S | 0.62 | 0.58 | 0.60 | 0.48 | 0.65 | 0.58 |

Table 4

Hydraulic indices of blast furnace slags, Rourkela

| Sl. No. | Formula | Slag Samples | | | | | | IS : 455-1976 requirements |
|---------|--|--------------|------|------|------|------|------|----------------------------|
| | | A | B | C | D | E | F | |
| 1. | $\frac{\text{CaO} + \text{MgO} + \frac{1}{3}\text{Al}_2\text{O}_3}{\text{SiO}_2 + \frac{1}{3}\text{Al}_2\text{O}_3}$ | 1.00 | 0.94 | 0.82 | 0.80 | 0.93 | 0.77 | > 1.0 |
| 2. | $\frac{\text{CaO} + \text{MgO} + \text{Al}_2\text{O}_3}{\text{SiO}_2}$ | 2.19 | 1.82 | 1.64 | 1.61 | 1.78 | 1.66 | > 1.0 |
| 3. | $\frac{\text{CaO} + \text{CaS} + \frac{1}{2}\text{MgO} + \text{Al}_2\text{O}_3}{\text{SiO}_2 + \text{MnO}}$ | 1.97 | 1.59 | 1.48 | 1.36 | 1.51 | 1.39 | > 1.5 |

Table 6

Proportions of PFS cement produced using unprocessed phosphogypsum

| Slag Sample Designation | PFS composition | | Normal consistency (%) | Setting Time (minutes) | | Compressive Strength (kg/cm ²) | | | Autoclave Expansion (%) | | |
|-------------------------------|--------------------|-----|------------------------------|---------------------------|-------|---|-----|-----|-------------------------------|-----|-------|
| | S* | C | | Initial | Final | 1d | 7d | 28d | | | |
| A | 40 | 60 | 22.8 | 250 | 375 | 110 | 190 | 343 | 450 | 595 | 0.10 |
| | 50 | 50 | 23.5 | 285 | 390 | 102 | 170 | 305 | 435 | 600 | 0.12 |
| B | 40 | 60 | 22.0 | 220 | 265 | 92 | 117 | 275 | 405 | 598 | 0.20 |
| | 50 | 50 | 22.0 | 276 | 325 | 85 | 169 | 215 | 470 | 577 | 0.5 |
| C | 40 | 60 | 21.0 | 235 | 280 | 75 | 160 | 225 | 368 | 580 | 0.08 |
| | 50 | 50 | 21.5 | 305 | 380 | 70 | 145 | 215 | 375 | 505 | 0.11 |
| D | 40 | 60 | 23.0 | 240 | 300 | 95 | 185 | 250 | 390 | 565 | 0.11 |
| | 50 | 50 | 24.0 | 224 | 325 | 88 | 160 | 220 | 378 | 545 | 0.11 |
| E | 40 | 60 | 23.0 | 190 | 240 | 130 | 240 | 370 | 399 | 555 | 0.075 |
| | 50 | 50 | 23.0 | 215 | 255 | 126 | 205 | 317 | 360 | 575 | 0.090 |
| F | 40 | 60 | 22.5 | 188 | 238 | 115 | 200 | 280 | 345 | 570 | 0.10 |
| | 50 | 50 | 23.5 | 195 | 248 | 105 | 180 | 299 | 355 | 512 | 0.10 |
| G | 0 | 100 | 22.0 | 180 | 225 | 144 | 260 | 305 | 592 | 611 | 0.30 |

* S = Slag

C = Cement clinker

UPG = Unprocessed phosphogypsum

† = Mineral Selenite Gypsum

The autoclave expansion was also within the specified limit of 0.8% maximum.

With Unprocessed Phosphogypsum: The use of unprocessed phosphogypsum as an additive to PBFS cement adversely affected the setting time and compressive strength (Table 6,

As can be seen, the setting time was prolonged and the compressive strength was decreased at 1, 3 & 7 days respectively. However, the later age strength at 28 and 90 days was not affected appreciably. In fact, later age (90 days) strength was nearly similar to that obtained with mineral selenite gypsum. The autoclave expansion values were within specified value of 0.8% maximum.

The retardation of setting is due to the water-soluble impurities of phosphogypsum which enter gradually into aqueous phase of hydrating cement paste. Among impurities of phosphates and fluorides, the water-soluble fluorides retard the setting time to a relatively greater extent. This observation confirms the findings of Kobayashi²³, Mori and Sudo⁶ who used monocalcium phosphate, dicalcium phosphate and sodium silico fluoride as the representative water soluble impurities and found greater retardation in setting time with sodium silico fluoride than mono or dicalcium phosphate. The extent of retardation was in proportion to the amount of impurities incorporated into the cement.

The rate of retardation was found to be more pronounced in case of PBFS cement than portland cement. It was further observed that while sodium silico fluoride alone prolonged the setting time greatly, its mixture with phosphates caused further

retardation. The presence of small amount of organic matter showed no ill effect on setting, but when present with phosphates and fluorides, the setting was greatly prolonged.

The impurities in phosphogypsum react with lime released by hydration of cement to form insoluble calcium salts ($\text{Ca}_3(\text{PO}_4)_2$ & CaF_2) which coat the cement particles, thereby preventing their hydration in the initial stages. c) **With Processed Phosphogypsum:** The properties of PBFS cement produced using processed phosphogypsum (wet sieved through 150 micron IS sieve and washed) are shown in Table 7. It can be seen that the use of processed phosphogypsum accelerated the setting time and increased the compressive strength at 1, 3 & 7 days.

The level of strength obtained was more or less similar to that attained with mineral gypsum. The later age strength at 28 & 90 days was not affected appreciably. The autoclave expansion data was within the specified limit of 0.8% maximum. The processed phosphogypsum is thus suitable for use in place of mineral selenite gypsum.

Conclusions

From the present investigation, it can be concluded that processed phosphogypsum (wet sieved through 150 micron IS sieve and washed) can be used in place of mineral selenite gypsum. Being available in the eastern and southern parts of the country where mineral selenite gypsum is not available, the use of processed phosphogypsum would be a definite economic advantage.

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Table 7

Properties of PPGs cement produced using processed phosphogypsum

| Slag Designation | PPG [*] : cement composition | | Thickness (mm) | Normal consistency (%) | Setting Time (minutes) | | Compressive Strength (kg/cm ²) | | | Autoclave Expansion (%) | | |
|------------------|---------------------------------------|-----|----------------|------------------------|------------------------|-------|--|-----|-----|-------------------------|-----|------|
| | S | C | | | Initial | Final | 1d | 3d | 7d | | 28d | 90d |
| A | 40 | 60 | 4009 | 23.0 | 190 | 250 | 147 | 220 | 405 | 470 | 615 | 0.10 |
| | 50 | 50 | 4000 | 23.5 | 250 | 320 | 141 | 220 | 350 | 450 | 625 | 0.10 |
| B | 40 | 60 | 4200 | 22.2 | 180 | 220 | 124 | 190 | 315 | 499 | 632 | 0.15 |
| | 50 | 50 | 4100 | 22.9 | 235 | 290 | 121 | 180 | 290 | 490 | 588 | 0.18 |
| C | 40 | 60 | 4100 | 22.0 | 185 | 240 | 110 | 180 | 280 | 430 | 640 | 0.10 |
| | 50 | 50 | 4064 | 22.0 | 290 | 370 | 100 | 170 | 255 | 400 | 555 | 0.10 |
| D | 40 | 60 | 4000 | 23.0 | 230 | 260 | 124 | 195 | 275 | 420 | 600 | 0.08 |
| | 50 | 50 | 4085 | 23.5 | 210 | 275 | 108 | 175 | 280 | 406 | 599 | 0.08 |
| E | 40 | 60 | 4100 | 23.0 | 160 | 230 | 166 | 270 | 410 | 521 | 600 | 0.10 |
| | 50 | 50 | 4147 | 24.0 | 180 | 230 | 154 | 218 | 325 | 522 | 580 | 0.10 |
| F | 40 | 60 | 4009 | 24.0 | 170 | 228 | 138 | 215 | 325 | 370 | 620 | 0.10 |
| | 50 | 50 | 4200 | 22.0 | 180 | 235 | 129 | 199 | 340 | 385 | 551 | 0.10 |
| | 0 | 100 | 3111 | 22.0 | 180 | 225 | 144 | 260 | 305 | 592 | 616 | 0.30 |

* S = Slag

C = Cement clinker

PPG = Processed phosphogypsum (wet sieved through 150 micron IS sieve and washed)

† = Mineral selenite gypsum

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